## OCR Maths M2

# Topic Questions from Papers 

## Centre of Mass

Answers

| $\mathbf{1}$ | (i) | use of $\mathrm{h} / 4$ | B1 |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | com vert above lowest pt of contact | B1 |  | can be implied |  |
|  |  | $\mathrm{r}=5 \times \tan 24^{\circ}$ | M1 |  |  |  |
|  |  | $\mathrm{r}=2.2$ | A1 | 4 | 2.226 |  |
|  | (ii) | No \& valid reason $\left(\mathrm{eg} 24^{\circ} \measuredangle 26.6^{\circ}\right)$ | B1 $\sqrt{ }$ | 1 | $\sqrt{ }$ Yes if their $\mathrm{r} \bullet 2.5$ | $\mathbf{5}$ |

(Q1, June 2005)

| $\mathbf{2}$ | (iii) | $1.6 \bar{y}=$ | M1 |  | must be moments with vert dists |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | $20 \times 0.2+20 \times 0.2+40 \times 0.5$ | A1 |  | or $1.6 \bar{y}=20 \times 0.2 \times 2+40 \times 0.7(22.5)$ |  |
|  |  | $\bar{y}=17.5 \mathrm{~cm}$ | A 1 | 3 |  |  |

(Q4, Jan 2006)

(Q3, June 2006)

| 4 | (i) | $\bar{x}=9$ <br> c of $m$ of $\Delta 4 \mathrm{~cm}$ above BD $\begin{aligned} & (324+108)(\mathrm{m}) \bar{y}= \\ & 324(\mathrm{~m}) \times 9+108(\mathrm{~m}) \times(18+4) \\ & 432 \bar{y} \\ & 324 \times 9 \quad\left(18^{2} \times 9\right) \\ & 108 \times(18+4) \\ & \bar{y}=12.25 \end{aligned}$ | B1 <br> B1 <br> M1 <br> A1 <br> A1 <br> A1 <br> A1 | 7 | ignore any working <br> 8 cm below C/see their diagram $432 \bar{y}=108 \times 8+18^{2}(12+9)$ <br> from C <br> left hand side <br> $1^{\text {st }}$ term on right hand side 2916 <br> $2^{\text {nd }}$ term on right hand side 2376 <br> $5292 \div 432$ or 49/4 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (ii) | $\begin{aligned} & \tan \theta=5.75 / 9^{\circ} \\ & \theta=32.6^{\circ} \text { or } 147.4^{\circ} \end{aligned}$ | $\begin{aligned} & \mathrm{M} 1 \\ & \mathrm{~A} 1 \delta \end{aligned}$ | 2 | $\begin{aligned} & \text { must be .../9 } \\ & \left.\left.\sqrt{\tan ^{-1}((18-t h e i r ~} \bar{y}\right) / 9\right) \text { or } 180^{\circ} . \end{aligned}$ |  |

(Q5, June 2006)

| $\mathbf{5}$ |  | com directly above lowest point | B1 |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | $\tan \alpha=6 / 10$ | M1 |  |  |  |
|  |  | $\alpha=31.0$ | A1 | 3 | or 0.540 rads | $\mathbf{3}$ |


| 6 | (i) | com of $\Delta 4 \mathrm{~cm}$ right of $C$ | B1 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $1.5 \times 10+7 \times 20=\bar{x} \times 30$ | M1 |  |  |  |
|  |  |  | A1 |  |  |  |
|  |  | $\bar{x}=5.17$ | A1 |  | $51 / 6$ 31/6 |  |
|  |  | com of $\Delta 6 \mathrm{~cm}$ above $E$ $4.5 \times 10+6 \times 20=\bar{y} \times 30$ | B1 |  | or 3 cm below $C$ |  |
|  |  | $4.5 \times 10+6 \times 20=\bar{y} \times 30$ | M1 |  |  |  |
|  |  |  | A1 |  |  |  |
|  |  | $\bar{y}=5.5$ | A1 | 8 |  |  |
|  | (ii) | $\tan \theta=5.17 / 3.5$ | M1 |  | right way up and (9- $\bar{y}$ ) |  |
|  |  | $55.9{ }^{\circ}$ or $124^{\circ}$ | A1/ | 2 | $\int$ their $\bar{x} /(9-\bar{y})$ |  |
|  | (iii) | $\mathrm{d}=15 \sin 45^{\circ} \quad(10.61)$ | B1 |  | dist to line of action of T |  |
|  |  | $\mathrm{Td}=30 \times 5.17$ | M1 |  | allow Tx15 i.e. T vertical |  |
|  |  | $\mathrm{T}=14.6$ | A1 | 3 |  | 13 |

(Q6, Jan 2007)

| $\mathbf{7}$ | com of hemisphere 0.3 from $O$ | B1 | or 0.5 from base |
| :--- | :--- | :--- | :--- |
|  | com of cylinder $h / 2$ from $O$ | B1 |  |
|  | $0.6 \times 45=40 \times 0.5+(0.8+h / 2) \times 5$ or | M1 | or $40 \times 0.3-5 \times h / 2=45 \times 0.2$ |
|  | $45(\mathrm{~h}+0.2)=5 \mathrm{~h} / 2+40(\mathrm{~h}+0.3)$ | A1 | or $5(0.2+\mathrm{h} / 2)=40 \times 0.1$ |
|  | $27=20+(0.8+h / 2) \times 5$ | M1 | solving |
|  | $h=1.2$ | A1 6 | AG |

(Q8, June 2007)

| 8 (i) | $\begin{aligned} & (2 x 4 x \sin \Pi / 2) / 3 \times \Pi / 2 \\ & 1.70 \\ & \hline \end{aligned}$ | $\begin{array}{ll} \hline \text { M1 } \\ \text { A1 } & 2 \\ \hline \end{array}$ | $\text { or } 4 \mathrm{r} / 3 \Pi$ AG |
| :---: | :---: | :---: | :---: |
| (ii)(a) | $\begin{array}{ll} \hline \bar{x} \times \mathrm{xd}\left(8 \times 20-\Pi \times 4^{2} / 2\right)=10 \times 8 \times 20 \mathrm{~d}- \\ 12 \times \Pi \times 4^{2} / 2 \times \mathrm{xd} \\ 10 \times 8 \times 20(\mathrm{~d}) & (1600) \\ \left(8 \times 20-\Pi \times 4^{2} / 2\right)(\mathrm{d}) & (134.9) \\ \left(12 \times \Pi \times 4^{2} / 2\right)(\mathrm{d}) \\ \bar{x}=9.63 \mathrm{~cm} \\ \hline \end{array}$ | M1  <br>   <br> A1  <br> A1  <br> A1  <br> A1 5 | $\begin{aligned} & \text { or } 134.9 \bar{x}= \\ & 64 \times 4+38.9 \times 12+32 \times 18 \quad(1298.8) \\ & 64 \times 4 \\ & 38.9 \times 12 \\ & 32 \times 18 \\ & \text { AG } \end{aligned}$ |
| (ii)(b) | $\begin{align*} & \bar{y} \times \mathrm{xd}\left(8 \times 20-\Pi \times 4^{2} / 2\right)=4 \mathrm{x} 8 \mathrm{x} 20 \mathrm{~d}- \\ & 1.7 \mathrm{x} \Pi \times 4^{2} / 2 \mathrm{xd} \\ & 4 \times 8 \times 20(\mathrm{~d}) \\ & 1.7 \mathrm{~d} \times \Pi \times 4^{2} / 2  \tag{13.6П}\\ & \bar{y}=4.43 \mathrm{~cm} \end{align*}$ | $\begin{aligned} & \text { M1 } \\ & \text { A1 } \\ & \text { A1M1 } \\ & \text { A1 } 4 \end{aligned}$ | or $64 \mathrm{x} 4=42.7+38.9 y$ $\begin{aligned} & \bar{y}=5.49 \\ & 135 \bar{y}=32 \times 4+38.9 \times 5.49+64 \times 4 \end{aligned}$ |

(Q8, Jan 2008)

| 9 (i) | $3 / 8 \times 3 \quad(1.125)$ | B1 | c.o.m. hemisphere |
| :--- | :--- | :--- | :--- |
|  | $0.53 \mathrm{~d}=5 \times 0.02+(10+3 / 8 \times 3) \times 0.5$ | M1 | $0.53 \mathrm{e}=3 \times 5 / 8 \times 0.5+8 \times 0.02+13 \times .01$ |
|  | $\mathrm{~d}=10.7$ | A1 | $0.53 \mathrm{f}=3 \times 3 / 8 \times 0.5-5 \times 0.02-10 \times 0.01$ |
|  | A1 4 | AG $(\mathrm{e}=2.316 \mathrm{f}=0.684)$ |  |


| 10 (i) | com of $\Delta 3 \mathrm{~cm}$ right of C | B1 |
| :--- | :--- | :--- |
|  | $(48+27) \bar{x}=48 \mathrm{x} 4+27 \mathrm{x} 11$ | M1 |
|  | $\bar{x}=6.52$ | A1 |
|  | A1 |  |
|  | com of $\Delta 2 \mathrm{~cm}$ above AD | B1 |
|  | $(48+27) \bar{y}=48 \times 3+27 \times 2$ | M1 |
|  | $\bar{y}=2.64$ | A1 |
|  | A1 8 |  |

(Q8, June 2008)

| 11 (ii) | $\mathrm{d}=(2 \mathrm{x} 40 \sin \Pi / 2) \div 3 \Pi / 2$ | M1 | must be radians |
| :---: | :---: | :---: | :---: |
|  |  | A1 |  |
|  | $\mathrm{d}=17.0$ | A1 | 16.98 160/3П (8/15П m ) |
|  | $70 \bar{y}=100 \times 60+217 \times 10$ | M1 |  |
|  |  | A1 ft | $\mathrm{ft} 200+$ their đ or $2+$ their đ (m) |
|  | $\bar{y}=117$ | A1 6 | 116.7 |

(Q3, Jan 2009)

(Q5, June 2009)

| 13 (i) | $\begin{aligned} & \overline{\mathrm{u}}=0.2 \text { (from vertex) or } 0.8 \text { or } 0.1 \\ & 0.5 \mathrm{~d}=0.2 \times \overline{\mathbf{u}}+0.3 \times 0.65 \end{aligned}$ $\mathrm{d}=0.47$ | B1  <br> M1  <br> A1  <br> A1 $[4]$ | com of conical shell AG |
| :---: | :---: | :---: | :---: |
| (ii) | $\begin{aligned} & \mathrm{s}=0.5 \\ & \mathrm{~T} \sin 80^{\circ} \times 0.5=0.47 \times 0.5 \times 9.8 \\ & \mathrm{~T}=4.68 \mathrm{~N} \end{aligned}$ | $\begin{array}{ll} \text { B1 } & \\ \text { M1 } & \\ \text { A1 } & \\ \text { A1 } & {[4]} \end{array}$ | slant height, may be implied |

(Q3, Jan 2010)

| 14 (i) | $\begin{aligned} & (6 \sin \Pi / 2) \div(\Pi / 2) \\ & 3.82 \end{aligned}$ | $\begin{aligned} & \text { M1 } \\ & \text { A1 } 2 \end{aligned}$ | Use of correct formula AG |
| :---: | :---: | :---: | :---: |
| (ii) | $\begin{aligned} & 8 \mathrm{~d}=3(6-3.82)+5 \mathrm{x} 9.82 \\ & \text { or } 8 \mathrm{x}= \pm\{3(-3.82)+5 \mathrm{x} 3.82\} \\ & \mathrm{d}=6.95 \text { or } 6.96 \text { or } \mathrm{x}=+/-0.955 \\ & \tan \theta=0.96 / 6 \\ & \theta=9^{\circ} \end{aligned}$ | M1 <br> A1 <br> A1 <br> M1 <br> A1 5 | Method to find centre of mass <br> Attempt to find the required angle 7 |

(Q2, June 2010)

| 15 | (i) | $\begin{aligned} & 3 \mathrm{x}_{\mathrm{G}}=2 \times 0.3+1 \times 0.6 \mathrm{OR} 3 \mathrm{x}_{\mathrm{G}}=2 \times 0.3+0 \mathrm{OR} 3 \mathrm{x}_{\mathrm{G}}=4 \times 0.3 \\ & \mathrm{OR} 3 \mathrm{y}_{\mathrm{G}}=1 \times 0.3+1 \times 0.6+0 \mathrm{OR} 3 \mathrm{y}_{\mathrm{G}}=4 \times 0.3-1 \times 0.3 \\ & \mathrm{x}_{\mathrm{G}}=0.4 \text { (from } \mathrm{AD} \text { ) OR } \mathrm{x}_{\mathrm{G}}=0.2 \quad \text { (from BC) } \\ & \mathrm{y}_{\mathrm{G}}=0.3 \mathrm{~m} \text { from } \mathrm{AB} \text { or } \mathrm{CD} \\ & \mathrm{AG}^{2}=0.4^{2}+0.3^{2} \\ & \mathrm{AG}=0.5 \mathrm{~m} \end{aligned}$ | M1 <br> A1 <br> A1 <br> M1 <br> A1 <br> [5] | Table of moments idea. M0 for reducing to 1D problem. Masses/weights may be included. <br> Pythagoras with 2 appropriate distances. <br> This may only be seen in (ii), allow M1A1 in this case. |
| :---: | :---: | :---: | :---: | :---: |

(Q1, Jan 2011)

| 16 | (i) | $\begin{aligned} & x_{H}=3 \times 0.6 / 8 \\ & \pi\left(0.6^{2} \times 0.6\right)(0.6 / 2)-\left(0.6^{3} \times 2 \pi / 3\right) 0.225 \\ & =\pi \times 0.6^{3}(1+2 / 3) x_{G} \\ & x_{G}=0.09 \mathrm{~m} \end{aligned}$ | B1 <br> M1 <br> A1 <br> A1 <br> A1 <br> [5] | CoM hemisphere ( $\mathrm{x}_{\mathrm{H}}=0.225$ ), may be implied Use of table of moments idea SC Volume of sphere used, max B1M1A1, moment equation fully correct for A1 (3/5) Accept -0.09 |
| :---: | :---: | :---: | :---: | :---: |

(Q5, Jan 2011)

| 17 i | $\begin{aligned} & -(8 \cos 30 / 3)\left(8^{2} \sin 60 / 2\right) \\ & +(4)\left(8^{2}\right) \\ & =\left(8^{2}+8^{2} \sin 60 / 2\right)\left(x_{G}\right) \\ & x_{G}=2.09 \mathrm{~cm} \end{aligned}$ | M1 <br> A1 <br> A1 <br> A1 <br> A1 <br> $[5]$ | Table of moments idea, may include g and/or density. $-2.309 \times 27.7$ |
| :---: | :---: | :---: | :---: |
| ii | $\begin{aligned} & \tan \theta=(2.09 / 4) \\ & \theta=27.6^{\circ} \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { M1 } \\ \text { A1ft } \\ \text { [2] } \end{array}$ | $\mathrm{ft} \mathrm{cv}\left(\mathrm{x}_{\mathrm{G}}\right)$ |

(Q3, June 2011)

| 18 | (i) | $\begin{aligned} & h=r \tan \alpha \\ & x\left(\frac{2}{3} \pi r^{3}+\frac{1}{3} \pi r^{2} h\right)=\frac{1}{3} \pi r^{2} h \times \frac{h}{4}-\frac{2}{3} \pi r^{3} \times \frac{3}{8} r \\ & x=\frac{r(\tan 2}{8+4-3)} \end{aligned}$ | $\begin{aligned} & \text { B1 } \\ & \text { M1 } \\ & \text { A1 } \\ & \text { A1 } \\ & {[4]} \end{aligned}$ | Seen anywhere and in any form. Table of values idea. <br> AG <br> www |
| :---: | :---: | :---: | :---: | :---: |
|  | (ii) | $\begin{aligned} & x<0 \\ & \text { Solve } \tan ^{2} \alpha-3<0 \\ & \alpha<60 \end{aligned}$ | $\begin{aligned} & \mathrm{B} 1 \\ & \mathrm{M} 1 \\ & \mathrm{~A} 1 \\ & {[3]} \end{aligned}$ | ```May be implied. Condone \(=\) Condone \(\leq\) throughout. SC Use of \(=\) or \(>\) throughout. Max B0 M1 A0``` |


| 19 | (i) | $\begin{aligned} & 1 / 3 a \\ & (25+2.5 a) x_{G} \\ & =25 \times 2.5+2.5 a \times(5+1 / 3 a) \\ & x_{\mathrm{G}}=\frac{a^{2}+15 a+75}{3(a+10)} \quad \mathbf{A G} \end{aligned}$ | $\begin{aligned} & \text { B1 } \\ & \text { M1 } \\ & \text { A1 } \\ & \text { A1 } \\ & \text { A1 } \\ & \text { [5] } \end{aligned}$ | Centre of mass of triangle Table of values idea, using any fixed axis Relative to the axis they are using |
| :---: | :---: | :---: | :---: | :---: |
|  | (ii) | $\frac{a^{2}+15 a+75}{3(a+10)}=5$ <br> Solving for $a$ $a=8.66 \text { or } 5 \sqrt{ } 3$ | $\begin{gathered} \text { *M1 } \\ \\ \text { dep*M1 } \\ \text { A1 } \\ {[3]} \\ \hline \end{gathered}$ | Substitute $x_{\mathrm{G}}$ as 5 $a \leq 8.66$ |
|  | (iii) | $\begin{aligned} & (25+2.5 a) y_{\mathrm{G}}=25 \times 2.5+2.5 a \times(2 / 3 \times 5) \\ & y_{\mathrm{G}}=\frac{10 a+75}{3(a+10)} \text { or } 2.89 \\ & \tan \theta=x_{\mathrm{G}} y_{\mathrm{G}} \\ & \quad=5 / y_{\mathrm{G}} \\ & \theta=60 \end{aligned}$ | $\begin{gathered} \text { *M1 } \\ \text { A1ft } \\ \text { A1ft } \\ \\ \text { dep*M1 } \\ \text { A1ft } \\ \text { A1 } \\ {[6]} \end{gathered}$ | Method to find centre of mass from $A B$ (or $C D$ ) with or without $a$ substituted. <br> ft their $a$ from (ii), from $\mathrm{CD} y_{\mathrm{G}}=2.11$ <br> Using trig to find an appropriate angle, eg complement of $\theta$. ft their $a$ from (ii), but not an incorrect $y_{\mathrm{G}}$ $\theta \leq 60$ (anything that rounds to 60 ) |

(Q7, June 2012)

| 20 | (i) | $\begin{aligned} & (2 \times 3 \sin (\pi / 2)) /(3 \pi / 2) \text { or equivalent } \\ & 3 \times 6^{2} \\ & -\left(\pi \times 3^{2} / 2\right) \times(6-4 / \pi) \\ & =\left(6^{2}-\pi \times 3^{2} / 2\right) \mathrm{x}_{\mathrm{G}} \\ & \mathrm{x}_{\mathrm{G}}=1.88 \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & \text { B1 } \\ & \text { M1 } \\ & \text { A1 } \\ & \text { A1 } \\ & \text { A1 } \\ & \text { A1 } \\ & {[6]} \end{aligned}$ | Centre of mass of semicircle; $4 / \pi$ Table of moments idea about any axis. |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | (ii) | $\begin{aligned} & \tan \theta=1.88 / 3 \\ & \theta=32.1^{\circ} \end{aligned}$ | $\begin{gathered} \hline \text { M1 } \\ \text { A1ft } \\ {[2]} \end{gathered}$ | Attempt at a relevant angle allow $180-\theta$ \& radians ( 0.561 or 0.560 ) |  |

(Q4, Jan 2013)

| 21 | (i) | $\begin{aligned} & 4.4 x_{\mathrm{G}}=4 \times 1 / 4 \times 8 \\ & \quad-0.4 \times 1 / 3 \times 10 \\ & x_{\mathrm{G}}=1.52 \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & \hline \text { M1 } \\ & \text { A1 } \\ & \text { A1 } \\ & \text { A1 } \\ & {[4]} \\ & \hline \end{aligned}$ | Table of moments idea. Moments about other axes acceptable $\text { Allow }{ }^{50} / 33$ |
| :---: | :---: | :---: | :---: | :---: |
|  | (ii) | $\begin{aligned} & T_{\text {shell }} \times 18=4.4 \mathrm{~g} \times(8-1.52) \text { or } T_{\text {cone }} \times 18=4.4 \mathrm{~g} \times(10+1.52) \\ & T_{\text {shell }}+T_{\text {cone }}=4.4 \mathrm{~g} \\ & T_{\text {shell }}=15.5 \text { and } T_{\text {cone }}=27.6 \end{aligned}$ | $\begin{gathered} \hline \text { M1 } \\ \text { A1ft } \\ \text { M1 } \\ \text { A1 } \\ {[4]} \\ \hline \end{gathered}$ | Or any other correct moment equation. ft on $x_{\mathrm{G}}$ from (i) May use a second moments equation For both |

